

ESCI 340 - Cloud Physics and Precipitation Processes  
Lesson 6 - Growth of Cloud Droplets by Diffusion  
Dr. DeCaria

## References:

*A Short Course in Cloud Physics, 3rd ed.*, Rogers and Yau, Ch. 7

## Flux

- A **flux** is the amount of something passing through a unit of area in a unit of time.
- The units of flux are the units of whatever is being transported, divided by area and time. Examples are:

**Mass flux:**  $\text{kg m}^{-2} \text{s}^{-1}$

**Energy flux:**  $\text{J m}^{-2} \text{s}^{-1}$

**Particle flux:**  $\text{m}^{-2} \text{s}^{-1}$

- The flux is actually a vector that points in the direction of the transport.
- In component form in Cartesian coordinates the flux vector is

$$\vec{F} = F_x \hat{i} + F_y \hat{j} + F_z \hat{k}. \quad (1)$$

## Fick's Laws of Diffusion

**NOTE:** *My notation for number of particles and number density differs from Rogers and Yau. I use  $N$  for number density, and  $n$  for number of particles.*

- **Fick's First Law of Diffusion** states that for particles the flux is always opposite to the gradient of the particle concentration (given as number density,  $N$ , in units of particles per cubic meter).
- Mathematically, Fick's First Law is written as

$$\vec{F} = -D\nabla N, \quad (2)$$

where  $D$  is the **diffusivity**.

– Diffusivity has units of  $\text{m}^2 \text{s}^{-1}$ .

- Figure 1 shows a rigid volume with flux vectors entering through the left face and leaving through the right face.

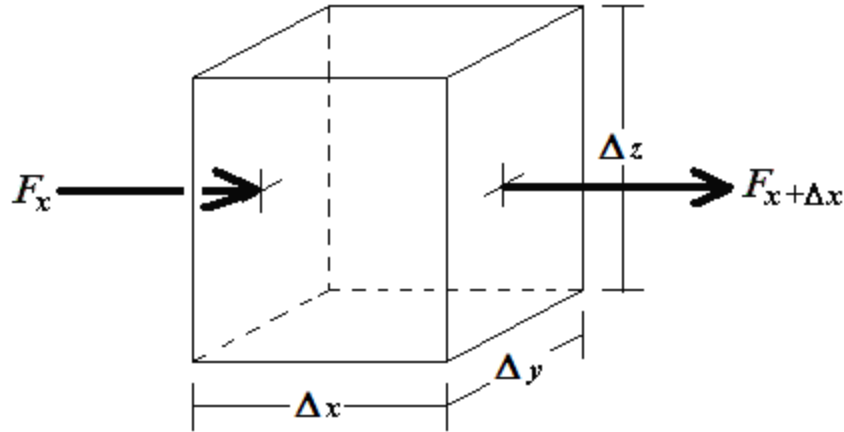


Figure 1: Flux vectors entering and leaving a volume from the  $x$ -oriented faces.

- The rate at which particles are entering through the left face is given by  $F_x \Delta y \Delta z$ .
- The rate at which particles are leaving through the right face is given by  $-F_{x+\Delta x} \Delta y \Delta z$ .
- The net change in number of particles  $n$  in the volume is therefore

$$\frac{\partial n}{\partial t} = -F_{x+\Delta x} \Delta y \Delta z + F_x \Delta y \Delta z = -(F_{x+\Delta x} - F_x) \Delta y \Delta z. \quad (3)$$

- In terms of number density,  $N$ , we have

$$\frac{\partial N}{\partial t} = \frac{1}{\Delta x \Delta y \Delta z} \frac{\partial n}{\partial t} = -\frac{1}{\Delta x \Delta y \Delta z} (F_{x+\Delta x} - F_x) \Delta y \Delta z = -\frac{F_{x+\Delta x} - F_x}{\Delta x}. \quad (4)$$

- In the limit as  $\Delta x \rightarrow 0$ , (4) becomes

$$\frac{\partial N}{\partial t} = -\frac{\partial F_x}{\partial x}. \quad (5)$$

- We could write similar expressions to (5) for the  $y$  and  $z$  directions, and combining the results would yield

$$\frac{\partial N}{\partial t} = -\frac{\partial F_x}{\partial x} - \frac{\partial F_y}{\partial y} - \frac{\partial F_z}{\partial z} = -\nabla \cdot \vec{F}. \quad (6)$$

- Equation (6) states that the change in number density in the volume depends on the divergence or convergence of the fluxes.
- If we combine (2) with (6) we get **Fick's Second Law of Diffusion**,

$$\frac{\partial N}{\partial t} = D \nabla^2 N, \quad (7)$$

which states that the rate of change of number density depends on the Laplacian of the number density.<sup>1</sup>

---

<sup>1</sup>Equation (7) is a differential equation known as the diffusion equation.

- To get a physical sense of what (7) means, let's look at it in the  $x$ -direction only,

$$\frac{\partial N}{\partial t} = \frac{\partial^2 N}{\partial x^2}. \quad (8)$$

- Figure (2) shows examples of the fluxes in the  $x$ -direction and how they relate to the second derivative of  $N$ .
  - When  $\partial^2 N/\partial x^2 > 0$  there is more flux entering than leaving the box, and so  $N$  will increase with time.
  - When  $\partial^2 N/\partial x^2 < 0$  there is more flux leaving than entering the box, and so  $N$  will decrease with time.
  - When  $\partial^2 N/\partial x^2 = 0$  there are equal amounts of flux entering and leaving the box, and so  $N$  will not change.

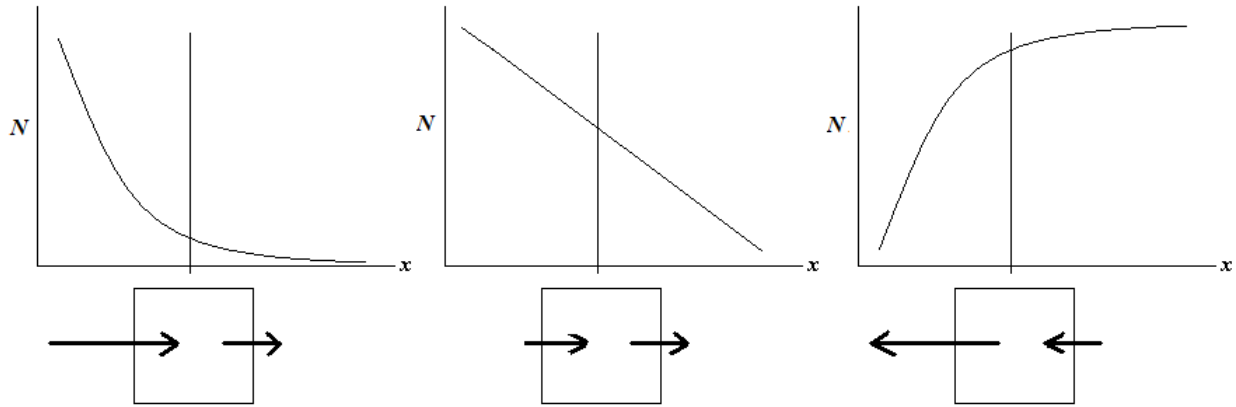


Figure 2: Graph showing the relationship between  $\partial^2 N/\partial x^2$  and the flux vectors entering and leaving a volume from the  $x$ -oriented faces.

## Growth Rate of Droplet by Diffusion

- Once a cloud droplet forms it continues to grow by diffusion of water vapor onto its surface (condensation).
- Figure 3 illustrates a droplet of radius  $R$  with radial vapor fluxes at the surface of the droplet denoted by  $\vec{F}_R$ .

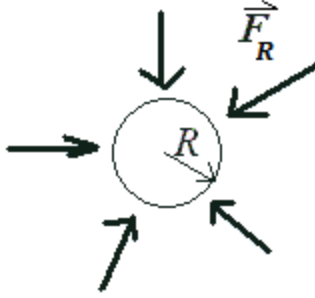


Figure 3: Convergence of radial vapor fluxes,  $\vec{F}_R$ , at the surface of the droplet results in droplet growth.

- For simplicity we will assume that the fluxes are *axisymmetric*, meaning that the fluxes only change with distance from the droplet, not with the angle. Another way of saying this is that the fluxes are *isotropic*.
- If we multiply the flux at the surface of the droplet by the surface area of the droplet we obtain the rate of change of molecules of the droplet,

$$\frac{dn}{dt} = -4\pi R^2 F_R. \quad (9)$$

- Note that  $F_R$  itself is negative, since it is pointing inward toward the droplet. That is why there is a negative in front of (9), so that  $dn/dt$  will be positive.

- The flux,  $F_R$ , at the surface of the droplet is given by Fick's first law of diffusion, (2), and is  $F_R = -\hat{k} \cdot D(\nabla N)_R = -D(\partial N/\partial r)_R$ .<sup>2</sup> Therefore (9) becomes

$$\frac{dn}{dt} = 4\pi D R^2 \left( \frac{\partial N}{\partial r} \right)_R. \quad (10)$$

- Keep in mind that  $n$  is the number of water molecules in the droplet itself, whereas  $N$  is the number density of water vapor molecules in the air.
- We find  $(\partial N/\partial r)_R$  as follows:
  - We assume that  $N$  does not change with time, so that from Fick's second law of diffusion, (7), we have

$$\nabla^2 N = 0. \quad (11)$$

---

<sup>2</sup>In spherical coordinates  $\nabla N = \frac{\hat{i}}{r \sin \varphi} \frac{\partial N}{\partial \theta} + \frac{\hat{j}}{r} \frac{\partial N}{\partial \varphi} + \hat{k} \frac{\partial N}{\partial r}$ , where  $\varphi$  is zenith angle and  $\theta$  is azimuth angle. Fortunately we only need the  $\hat{k}$  component.

- In spherical coordinates with the droplet at the origin, and since the vapor concentration is axisymmetric, (11) becomes<sup>3</sup>

$$\frac{\partial}{\partial r} \left( r^2 \frac{\partial N}{\partial r} \right) = 0. \quad (12)$$

- Integrating (12) twice with respect to  $r$  results in

$$N(r) = -\frac{c_1}{r} + c_2, \quad (13)$$

where  $c_1$  and  $c_2$  are the constants of integration. We find them by applying the boundary conditions

$$\begin{aligned} N(r \gg R) &= N_b \\ N(R) &= N_R. \end{aligned} \quad (14)$$

where  $N_b$  is the background vapor concentration well away from the droplet.<sup>4</sup>

- Applying the boundary conditions (14) to (13) results in

$$\begin{aligned} c_1 &= (N_b - N_R)R \\ c_2 &= N_b. \end{aligned}$$

- Putting these constants back into (13) results in

$$N(r) = -\frac{(N_b - N_R)R}{r} + N_b. \quad (15)$$

- And finally, by taking  $\partial/\partial r$  of (15) and evaluating the result at  $r = R$ , we get that

$$\left( \frac{\partial N}{\partial r} \right)_R = \frac{N_b - N_R}{R}. \quad (16)$$

- Putting (16) into (10) gives us our growth-rate equation for the droplet,

$$\frac{dn}{dt} = 4\pi DR(N_b - N_R). \quad (17)$$

- If the background vapor concentration is larger than that at the droplet surface,  $N_b > N_R$ , the droplet will grow due to condensation.
- If the background vapor concentration is smaller than that at the droplet surface,  $N_b < N_R$ , the droplet will shrink due to evaporation.

---

<sup>3</sup>In spherical coordinates  $\nabla^2 N = \frac{1}{r^2 \sin^2 \varphi} \frac{\partial}{\partial \varphi} \left( \sin \varphi \frac{\partial N}{\partial \varphi} \right) + \frac{1}{r^2 \sin^2 \varphi} \frac{\partial^2 N}{\partial \theta^2} + \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial N}{\partial r} \right)$ , but with axisymmetry the only non-zero term is the last one.

<sup>4</sup>Rogers and Yau use  $n_\infty$  instead of  $N_b$ .

## Growth Rate in Terms of Droplet Mass and Radius

- Equation (17) can be converted to an equation for the mass growth rate,  $dm/dt$ , as follows:

- Multiply both sides of (17) by the molar mass of water,  $M_w$ , and divide by Avogadro's number,  $N_A$ ,

$$\frac{M_w}{N_A} \frac{dn}{dt} = \frac{M_w}{N_A} 4\pi DR(N_b - N_R). \quad (18)$$

- Since mass is

$$\frac{M_w}{N_A} n = m$$

and absolute humidity is

$$\frac{M_w}{N_A} N = \rho_v,$$

(18) becomes

$$\frac{dm}{dt} = 4\pi DR(\rho_{vb} - \rho_{vR}). \quad (19)$$

- What would be most convenient is to have an equation for the growth-rate in terms of the radius of the droplet. We can construct this using the chain rule for derivatives,

$$\frac{dR}{dt} = \frac{dR}{dm} \frac{dm}{dt}. \quad (20)$$

- The mass of a droplet is

$$m = \frac{4}{3}\pi\rho_l R^3,$$

so

$$\frac{dR}{dm} = \frac{1}{4\pi\rho_l R^2}. \quad (21)$$

- From (19), (20) and (21) we get

$$R \frac{dR}{dt} = \frac{D}{\rho_l} (\rho_{vb} - \rho_{vR}). \quad (22)$$

## Other Equations Needed to Solve for Growth Rate

- Equation (22) gives us the ability to integrate forward in time to find an expression for  $R(t)$ , the radius of the droplet at any future time  $t$ .
  - We do not know what value of  $\rho_{vR}$  to use, since this depends on the temperature of the surface of the droplet.
  - However, we can assume that at the surface of the droplet the air is saturated, so that  $\rho_{vR} = \rho_{vs}$ , where  $\rho_{vs}$  is the *saturation absolute humidity*.

- From the ideal gas law for water vapor

$$\rho_{vR} = \rho_{vs} = \frac{e_s}{R_v T_R} \quad (23)$$

where  $T_R$  is the temperature at the surface of the droplet.

- \* Note that  $T_R$  is not necessarily the same as the air temperature. The droplet warms or cools depending on whether there is condensation or evaporation at the droplet's surface.

- $e_s$  is the saturation vapor pressure over a curved, impure droplet which we know to be

$$e_s = e_0 \left( 1 + \frac{a}{R} - \frac{b}{R^3} \right) \exp \left[ \frac{L_v}{R_v} \left( \frac{1}{T_0} - \frac{1}{T_R} \right) \right], \quad (24)$$

so that

$$\rho_{vR} = \frac{e_0}{R_v T_R} \left( 1 + \frac{a}{R} - \frac{b}{R^3} \right) \exp \left[ \frac{L_v}{R_v} \left( \frac{1}{T_0} - \frac{1}{T_R} \right) \right]. \quad (25)$$

- Equations (22) and (25) are two equations, but we have three unknown quantities:  $R$ ,  $\rho_{vR}$ , and  $T_R$ . Therefore we still need one more equation in order to have a closed set that we can solve.
- The third equation comes from balancing the gain of latent heat due to condensation with the loss of sensible heat due to thermal diffusivity.

- The gain of latent heat due to condensation is given by

$$J_{latent} = L_v \frac{dm}{dt} = 4\pi R L_v D (\rho_{vb} - \rho_{vR}). \quad (26)$$

- The sensible lost to the air by diffusion is

$$J_{sensible} = -4\pi R K (T_R - T_b), \quad (27)$$

where  $K$  is the thermal diffusivity of air and  $T_b$  is the temperature of the air.

- The sensible heat loss and latent heat gain must sum to zero in equilibrium, and so summing (26) and (27) and setting them equal to zero results in

$$\rho_{vb} - \rho_{vR} = \frac{K}{L_v D} (T_R - T_b). \quad (28)$$

## Calculations of Growth Rates

- Equations (22), (25) and (28) are three equations for three unknown quantities,  $R$ ,  $\rho_{vR}$ , and  $T_R$ . The equations are rewritten here,

$$\begin{aligned} R \frac{dR}{dt} &= \frac{D}{\rho_l} (\rho_{vb} - \rho_{vR}) \\ \rho_{vR} &= \frac{e_0}{R_v T_R} \left( 1 + \frac{a}{R} - \frac{b}{R^3} \right) \exp \left[ \frac{L_v}{R_v} \left( \frac{1}{T_0} - \frac{1}{T_R} \right) \right] \\ \rho_{vb} - \rho_{vR} &= \frac{K}{L_v D} (T_R - T_b). \end{aligned}$$

- We can solve these three equations to find the growth rate and radius of a droplet at any future time,  $t$ .
- However, the equations are quite complex and cannot be solved analytically. They need to be solved numerically.
- A somewhat simplified, though not as accurate, set of growth equations is<sup>5</sup>

$$R \frac{dR}{dt} = \frac{S - 1 - \frac{a}{R} + \frac{b}{R^3}}{F_k + F_d} \quad (29)$$

$$F_k = \left( \frac{L_v}{R_v T_b} - 1 \right) \frac{L_v \rho_l}{K T_b} \quad (30)$$

$$F_d = \frac{\rho_l R_v T_b}{D e_{s\infty}^*}, \quad (31)$$

where the saturation vapor pressure used in calculating  $F_d$  is that for a flat surface of pure water.

- These equations still need to be integrated numerically. The result for a droplet starting at radius  $r_0 = 0.75 \mu\text{m}$  is shown in Fig. 4.
- Note that after 20 hours the droplet is still only has a radius slightly larger than  $60 \mu\text{m}$ .

---

<sup>5</sup>These equations are developed in *The Physics of Clouds* by Mason (1971).



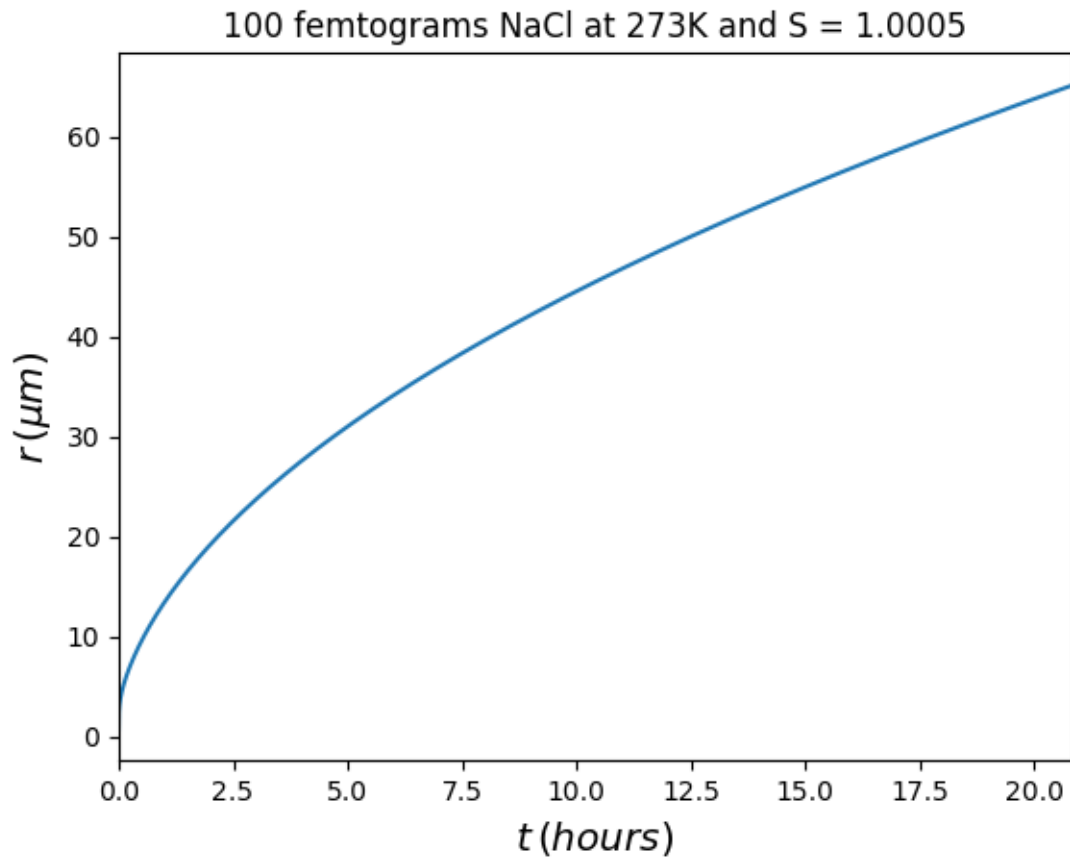


Figure 4: Growth of droplet initially of radius  $0.75 \mu\text{m}$  for a solute of 100 femtograms of NaCl.

- Fig. 5 shows the effect of doubling the mass of solute. Although the droplet initially grows faster with more solute, the growth rates quickly become the same.

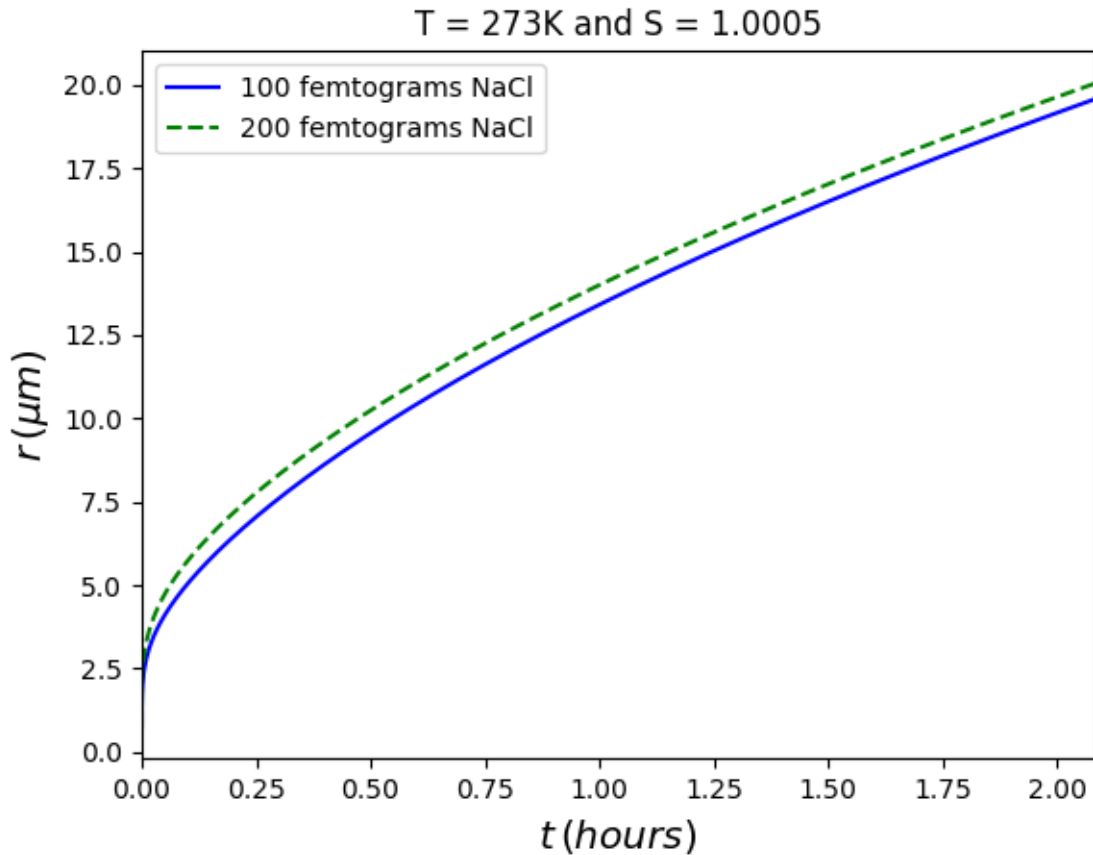


Figure 5: Growth of droplet initially of radius  $0.75 \mu\text{m}$  for two different solute masses.

## Final Comments on Diffusional Growth

- In order to be large enough to fall fast enough to reach the ground without evaporating, a droplet has to reach a size of at least  $0.1 \text{ mm}$  in diameter ( $0.05 \text{ mm}$  or  $50 \mu\text{m}$  in radius).
- A typical raindrop has a diameter of  $2 \text{ mm}$  (radius of  $1 \text{ mm}$ , or  $1000 \mu\text{m}$ ).
- Clouds can form and rain start to fall in a matter of 30 minutes or so.
- Diffusional growth explains how very tiny, brand-new cloud droplets grow to typical cloud droplet sizes, but is too slow to explain how precipitation forms.

## Exercises

1. For radii larger than a few microns the curvature and solute effects become negligible, and (29) becomes

$$R \frac{dR}{dt} = \frac{S - 1}{F_k + F_d}. \quad (32)$$

(a) Show that (32) can be analytically integrated to obtain

$$R(t) = \sqrt{R_0^2 + 2\xi t} \quad (33)$$

where  $\xi = (S - 1)/(F_k + F_d)$ .

(b) Use (33) to find how long it would take for a droplet to grow from an initial radius of 5 microns to a final radius of 50 microns for a saturation ratio of 1.0005 and a temperature of 273.15K. Use Table 7.1 on page 103 of Rogers and Yau to determine values for  $K$  and  $D$ . For  $L_v$  use  $2.5 \times 10^6 \text{ J kg}^{-1}$ .

2. Show that (22) can be written in terms of vapor pressure rather than absolute humidity

$$R \frac{dR}{dt} = \frac{D}{R_v \rho_l} \left( \frac{e_{sb}}{T_b} - \frac{e_{sR}}{T_R} \right). \quad (34)$$

3. Integrate

$$\frac{d}{dr} \left( r^2 \frac{dN}{dr} \right) = 0$$

and apply the boundary conditions

$$\begin{aligned} N(r \gg R) &= N_b \\ N(R) &= N_R \end{aligned}$$

to show that

$$N(r) = -\frac{(N_b - N_R)R}{r} + N_b.$$